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Transportation Noise Assessment

Hammond Road Duplication – Branch Circus to Bartram Road

Reference: 19055001-01.docx

Prepared for:

City of Cockburn



Report: 19055001-01.docx

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17-Sep-19	0	Noise walls included.	Terry George	-

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A Proposed Road Design

B Terminology

1 INTRODUCTION

City of Cockburn is proposing a duplication of Hammond Road, between Branch Circus and Bartram Road, located as shown in *Figure 1-1*. In this section, Hammond Road is single carriageway, with one lane in each direction. North of Branch Circus, the road is dual carriageway, with two lanes in each direction up until Beeliar Drive. Similarly, south of Bartram Road is also dual carriageway, two lanes in each direction until Russell Road. The proposed road design is provided in *Appendix A*.



Figure 1-1 Road Project Locality

This report considers the potential road traffic noise impacts associated with the duplication, in accordance with *State Planning Policy 5.4 Road and Rail Transport Noise and Freight Considerations in Land Use Planning*. The scope involved:

- Quantification of existing noise levels by noise monitoring at two locations;
- Setting up a noise model for existing conditions and calibrating against the noise monitoring (Existing Scenario);
- Use the calibrated noise model and modify for future traffic volumes on the existing road (No Build Scenario); and
- Use the calibrated noise model and modify for future traffic volumes on the proposed road design (Build Scenario).

Appendix B contains a description of some of the terminology used throughout this report.

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2 CRITERIA

The criteria relevant to this assessment is the *State Planning Policy 5.4 Road and Rail Transport Noise and Freight Considerations in Land Use Planning* (hereafter referred to as the Policy) produced by the Western Australian Planning Commission (WAPC). The objectives in the Policy are to:

- Protect people from unreasonable levels of transport noise by establishing a standardised set of criteria to be used in the assessment of proposals;
- Protect major transport corridors and freight operations from incompatible urban encroachment;
- Encourage best practice design and construction standards for new development proposals and new or redevelopment transport infrastructure proposals;
- Facilitate the development and operation of an efficient freight network; and
- Facilitate the strategic co-location of freight handling facilities.

For a major redevelopment, practicable noise management and mitigation measures should be considered, having regard to –

- The existing transport noise levels;
- The likely change in noise emissions resulting from the proposal; and
- The nature and scale of the works and potential for noise amelioration.

When considering the noise levels, the Policy's outdoor noise criteria, shown below in *Table 2-1*, can be used for some guidance. These criteria apply for new road projects rather than upgrades/modifications and at any point 1-metre from a ground floor habitable façade of a noise sensitive premises.

Table 2-1 Outdoor Noise Criteria

Period	Target	Limit
Day (6am to 10pm)	55 dB L _{Aeq(Day)}	60 dB L _{Aeq(Day)}
Night (10pm to 6am)	50 dB L _{Aeq(Night)}	55 dB L _{Aeq(Night)}

Note: The 5 dB difference between the target and limit is referred to as the margin.

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3 METHODOLOGY

Noise measurements and modelling have been undertaken in accordance with the requirements of the Policy as described in *Section 3.1* and *Section 3.2*.

3.1 Site Measurements

Noise monitoring was undertaken at two (2) locations between 21 July to 30 July 2019 in order to:

- Quantify the existing noise levels;
- Determine the differences between different acoustic parameters ($L_{A10,18hour}$, $L_{Aeq(Day)}$ and $L_{Aeq(Night)}$); and
- Calibrate the noise model for existing conditions.

The instruments used were ARL Ngara Type noise data loggers as follows:

- 1. Ngara 8780F6 at 14 Gandossi Court, Success (refer Figure 3-1); and
- 2. Ngara 87803e at 16 Muirfield Avenue, Success (refer Figure 3-2).

Each microphone was 1.4 metres above ground level with the logger programmed to record hourly L_{A1} , L_{A90} , and L_{Aeq} levels. The instruments comply with the requirements of *Australian Standard 2702-1984 Acoustics – Methods for the Measurement of Road Traffic Noise*. The loggers were field calibrated before and after the measurement session and found to be accurate to within +/- 1 dB. Lloyd George Acoustics also holds current laboratory calibration certificate for the loggers.







Figure 3-2 16 Muirfield Avenue

The noise data collected was verified by inspection and professional judgement. Where hourly data was considered atypical, an estimated value was inserted.

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3.2 Noise Modelling

The computer programme *SoundPLAN 8.1* was utilised incorporating the *Calculation of Road Traffic Noise* (CoRTN) algorithms, modified to reflect Australian conditions. The modifications included the following:

- Vehicles were separated into heavy (Austroads Class 3 upwards) and non-heavy (Austroads Classes 1 & 2) with non-heavy vehicles having a source height of 0.5 metres above road level and heavy vehicles having two sources, at heights of 1.5 metres and 3.6 metres above road level, to represent the engine and exhaust respectively. By splitting the noise source into three, allows for less barrier attenuation for high level sources where barriers are to be considered.
- Note that a -8.0 dB correction is applied to the exhaust and -0.8 dB to the engine (based on Transportation Noise Reference Book, Paul Nelson, 1987), so as to provide consistent results with the CoRTN algorithms for the no barrier scenario;
- An adjustment of -1.7 dB has been applied to the L_{Aeq(Day)} levels where noise levels are predicted to a facade, based on the findings of *An Evaluation of the U.K. DoE Traffic Noise Prediction*; Australian Road Research Board, Report 122 ARRB NAASRA Planning Group (March 1983).

Predictions are made at heights of 1.4 m above ground floor level and at 1.0 metre from an assumed building facade, resulting in a + 2.5 dB correction due to reflected noise.

Various input data are included in the modelling such as ground topography, road design, traffic volumes etc. These model inputs are discussed in the following sections.

3.2.1 Ground Topography & Road Design

General topography is on file from previous projects based on Landgate data. This data also contained building outlines for existing properties. This was checked against aerial photography and updated as necessary. Single storey houses are modelled as 3.5 metres high and double storey houses at 7.0 metres high.

The road design information was provided by City of Cockburn via email on 1 August 2019.

3.2.2 Traffic Data

Traffic data includes:

• Road Surface – The noise relationship between different road surface types is shown in *Table 3-1*.

Table 3-1 Noise Relationship Between Different Road Surfaces

Chip Seal				Asp	halt	
14mm	10mm	5mm	Dense Graded	Novachip	Stone Mastic	Open Graded
+3.5 dB	+2.5 dB	+1.5 dB	0.0 dB	-0.2 dB	-1.5 dB	-2.5 dB

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The existing road surface is dense graded asphalt and is assumed to be the same in the future.

- Vehicle Speed The existing and future posted speeds are generally 70km/hr. North of Branch Circus the posted speed is 60 km/hr. A school zone (2.30pm to 4.00pm 40 km/hr) exists between Makjanich Place and Windermere Circuit.
- Traffic Volumes Existing (2016) and forecast (2031) traffic volumes were provided by Main Roads WA (Clare Yu, Traffic Modelling Analyst, Reference: #41260, dated 01 August 2019). A validation plot was also provided allowing the Main Roads WA traffic volume model to be calibrated. *Table 3-2* provides the traffic volume input data in the model.

Table 3-2 Traffic Information Used in the Modelling for Hammond Road

	Scenario					
Section	Existing	g - 201 6	Future - 2031			
	Northbound	Southbound	Northbound	Southbound		
North of Branch Circus	3500 (8)	3100 (6)	5900 (8)	6600 (6)		
South of Branch Circus	3500 (8)	3100 (6)	5900 (8)	6600 (6)		
South of Bartram Road	5000 (8)	4700 (6)	4000 (7)	4200 (8)		

Notes:

3.2.3 Ground Attenuation

The ground attenuation has been assumed to be 0.0 (0%) for the road and 0.5 (50%) elsewhere. Note 0.0 represents hard reflective surfaces such as water and 1.00 represents absorptive surfaces such as grass.

3.2.4 Parameter Conversion

The CoRTN algorithms used in the *SoundPlan* modelling package were originally developed to calculate the $L_{A10,18hour}$ noise level. The WAPC Policy however uses $L_{Aeq(Day)}$ and $L_{Aeq(Night)}$. The relationship between the parameters varies depending on the composition of traffic on the road (volumes in each period and percentage heavy vehicles).

As noise monitoring was undertaken, the relationship between the parameters is based on the results of the monitoring – refer *Section 4.1*.

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^{1.} Numbers shown in brackets are % heavy vehicles obtained direct from ROM plots.

4 RESULTS

4.1 Noise Monitoring

The results of the noise monitoring are summarised in *Table 4-1* and *Table 4-2* and shown graphically in *Figure 4-1* and *Figure 4-2* for 14 Gandossi Court and 16 Muirfield Avenue respectively.

Table 4-1 Measured Average Noise Levels - 14 Gandossi Court

Date	Average Weekday Noise Level, dB				
Date	L _{A10,18hour}	L _{Aeq,24hour}	L _{Aeq (Day)}	L _{Aeq (Night)}	
Monday 22 July 2019	59.5	56.8	58.2	51.4	
Tuesday 23 July 2019	59.6	56.7	58.1	50.9	
Wednesday 24 July 2019	60.1	57.5	58.9	50.7	
Thursday 25 July 2019	58.7	56.6	58.0	50.7	
Friday 26 July 2019	59.1	56.1	57.6	49.7	
Monday 29 July 2019	57.8	55.1	56.3	50.6	
Weekday Average	59.1	56.5	57.8	50.7	

Table 4-2 Measured Average Noise Levels - 16 Muirfield Avenue

Data	Average Weekday Noise Level, dB				
Date	L _{A10,18hour}	L _{Aeq,24hour}	L _{Aeq (Day)}	L _{Aeq (Night)}	
Monday 22 July 2019	61.2	58.9	60.3	52.6	
Tuesday 23 July 2019	61.0	58.0	59.5	50.5	
Wednesday 24 July 2019	61.0	58.3	59.8	50.6	
Thursday 25 July 2019	60.9	59.0	60.6	50.8	
Friday 26 July 2019	60.9	58.0	59.6	49.8	
Monday 29 July 2019	59.6	57.0	58.3	51.8	
Weekday Average	60.8	58.2	59.7	51.0	

The results indicate that the $L_{Aeq(Night)}$ is around 8 dB less than the $L_{Aeq(Day)}$ so that the $L_{Aeq(Day)}$ parameter will determine compliance or otherwise. As such, the focus of this report will be the $L_{Aeq(Day)}$ noise levels.

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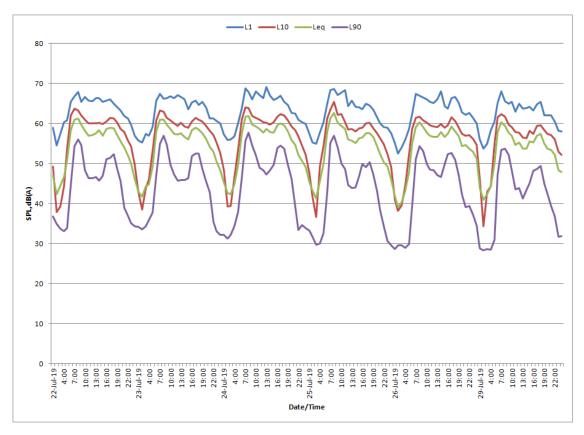


Figure 4-1 Noise Monitoring Results: 14 Gandossi Court

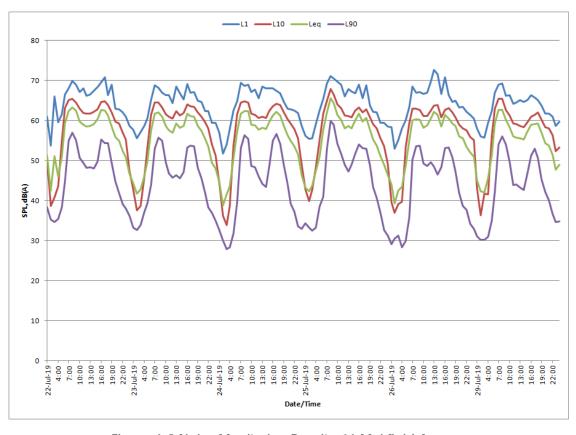


Figure 4-2 Noise Monitoring Results: 16 Muirfield Avenue

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4.2 Noise Modelling

Three scenarios are considered in noise modelling being Existing, No Build and Build and each are discussed in *Section 4.2.1* to *Section 4.2.3*.

4.2.1 Existing Scenario

The purpose of the Existing Scenario is to calibrate the noise model. The L_{Aeq(Day)} value is predicted to the two monitoring locations as shown in *Table 4-3* and compared against the measured noise levels of *Table 4-1* and *Table 4-2*. This difference becomes the calibration factor which is applied to the No Build and Build Scenario noise models.

LocationMeasured LAeq(Day), dBModelled LAeq(Day), dBDifference, dB14 Gandossi Court57.859.11.316 Muirfield Avenue59.759.80.1

Table 4-3 Model Calibration

The above shows that the model is over-predicting noise levels on average by 0.7 dB. As such, this factor has been applied to all three scenarios. On this basis, the model has an accuracy of \pm 0.6 dB to the noise monitoring locations.

Table 4-4 provides the predicted noise levels for the Existing Scenario to adjoining residences and this is also shown as noise contours on *Figure 4-3*.

Predicted **Predicted Address Address** L_{Aeq(Day)}, dB L_{Aeq(Day)}, dB **East Side Residences West Side Residences** 01 Condil Way 60 8 Muirfield Avenue 59 03 Condil Way 60 10 Muirfield Avenue 58 05 Condil Way 57 12 Muirfield Avenue 59 07 Condil Way 57 14 Muirfield Avenue 59 09B Condil Way 58 16 Muirfield Avenue (Logger) 59 1/1 Modong Nook 18 Muirfield Avenue 58 59 2/1 Modong Nook 57 20 Muirfield Avenue 59 57 22 Muirfield Avenue 58 3/1 Modong Nook 4/1 Modong Nook 57 24 Muirfield Avenue 58

Table 4-4 Predicted Laeq(Day) Noise Levels: Existing Scenario

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26 Muirfield Avenue

58

57

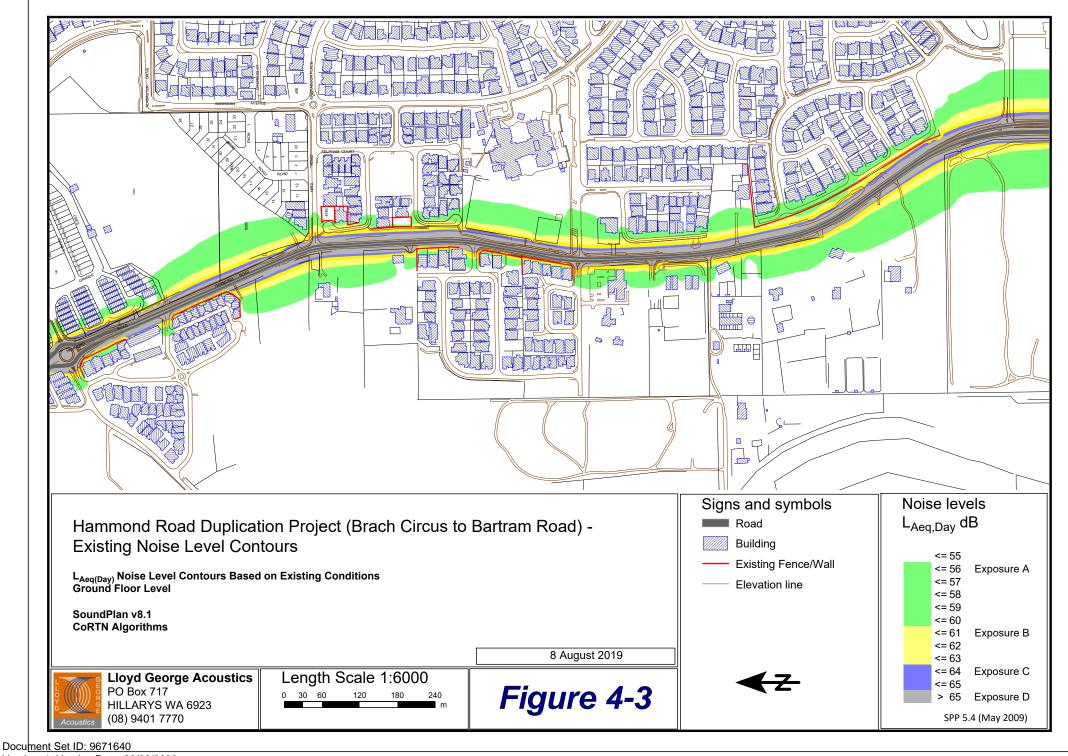
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5/1 Modong Nook

Address	Predicted L _{Aeq(Day)} , dB	Address	Predicted L _{Aeq(Day)} , dB	
West Side Residence	es	East Side Residences		
6/1 Modong Nook	57	28 Muirfield Avenue	56	
7/1 Modong Nook	57	40 Carnegie Parade	57	
8/1 Modong Nook	57	275 Hammond Road	54	
9/1 Modong Nook	57	17 Joindre Way	59	
9/1 Modong Nook	57	15 Joindre Way	60	
210 Hammond Road	57	11B Joindre Way	60	
222 Hammond Road	52	11A Joindre Way	60	
30 Calytrix Crescent	58	09 Joindre Way	59	
28 Calytrix Crescent	58	07 Joindre Way	59	
26 Calytrix Crescent	59	05B Joindre Way	58	
2 Aphelia Brace	61	05A Joindre Way	58	
2 Aphelia Brace	62	08 Joindre Way Goodstart Early Learning	59	
22 Calytrix Crescent	57	53 Baningan Avenue - Jandakot Primary	53	
20 Calytrix Crescent	57	15 Makjanich Place	56	
16 Calytrix Crescent	54	13 Makjanich Place	59	
21 Wedgetail Crescent	57	11B Makjanich Place	60	
25 Wedgetail Crescent	56	11A Makjanich Place	56	
27 Wedgetail Crescent	57	12 Makjanich Place	54	
272 Hammond Road	60	13 Gandossi Court	54	
282 Hammond Road	54	13 Gandossi Court	59	
300 Hammond Road	56	13 Gandossi Court	58	
304 Hammond Road	53	12A Gandossi Court	57	
	1	12A Gandossi Court	57	
		14 Gandossi Court (Logger)	58	
		01 Hird Road	57	
		01 Hird Road	59	
		01 Hird Road	57	

Note: Numbers shown in Bold Red are above the *limit*.

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4.2.2 No Build Scenario

The No Build Scenario assumes the existing road carries the 2031 traffic volumes. The outcome shows the increase in noise level as a result of increased traffic volumes only and represents the noise that will be present if the project does not occur, assuming the current road can carry the projected number of vehicles. The results are provided in *Table 4-5* and *Figure 4-4*.

Table 4-5 Predicted L_{Aeq(Day)} Noise Levels: No Build Scenario

Address	Predicted L _{Aeq(Day)} , dB	Address	Predicted L _{Aeq(Day)} , dB	
West Side Residence	es	East Side Residences		
01 Condil Way	63	8 Muirfield Avenue	61	
03 Condil Way	62	10 Muirfield Avenue	61	
05 Condil Way	60	12 Muirfield Avenue	61	
07 Condil Way	59	14 Muirfield Avenue	61	
09B Condil Way	61	16 Muirfield Avenue (Logger)	62	
1/1 Modong Nook	60	18 Muirfield Avenue	61	
2/1 Modong Nook	60	20 Muirfield Avenue	61	
3/1 Modong Nook	59	22 Muirfield Avenue	60	
4/1 Modong Nook	59	24 Muirfield Avenue	60	
5/1 Modong Nook	60	26 Muirfield Avenue	60	
6/1 Modong Nook	59	28 Muirfield Avenue	59	
7/1 Modong Nook	59	40 Carnegie Parade	60	
8/1 Modong Nook	59	275 Hammond Road	57	
9/1 Modong Nook	60	17 Joindre Way	62	
9/1 Modong Nook	60	15 Joindre Way	62	
210 Hammond Road	N/A	11B Joindre Way	62	
222 Hammond Road	53	11A Joindre Way	62	
30 Calytrix Crescent	60	09 Joindre Way	62	
28 Calytrix Crescent	60	07 Joindre Way	62	
26 Calytrix Crescent	61	05B Joindre Way	61	
2 Aphelia Brace	64	05A Joindre Way	61	
2 Aphelia Brace	65	08 Joindre Way Goodstart Early Learning	62	
22 Calytrix Crescent	60	53 Baningan Avenue - Jandakot Primary	56	
20 Calytrix Crescent	59	15 Makjanich Place	58	
16 Calytrix Crescent	56	13 Makjanich Place	62	

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Address	Predicted L _{Aeq(Day)} , dB	Address	Predicted L _{Aeq(Day)} , dB
West Side Residences		East Side Residences	
21 Wedgetail Crescent	59	11B Makjanich Place	62
25 Wedgetail Crescent	58	11A Makjanich Place	59
27 Wedgetail Crescent	59	12 Makjanich Place	56
272 Hammond Road	62	13 Gandossi Court	57
282 Hammond Road	57	13 Gandossi Court	62
300 Hammond Road	59	13 Gandossi Court	61
304 Hammond Road	55	12A Gandossi Court	60
		12A Gandossi Court	60
		14 Gandossi Court (Logger)	61
		01 Hird Road	60
		01 Hird Road	62
		01 Hird Road	60

Note: Numbers shown in Bold Red are above the *limit*.

Note that the existing residence at 210 Hammond Road is to be demolished and a Medical Centre constructed. Residential apartments will also form part of the new development, however if these are affected by road traffic noise, this will be the developers responsibility by way of facade upgrades and the like.

4.2.3 Build Scenario

The Build Scenario represents the future traffic volumes on the proposed road design. The results are provided in *Table 4-6* and *Figure 4-5*.

Table 4-6 Predicted LAeq(Day) Noise Levels: Build Scenario

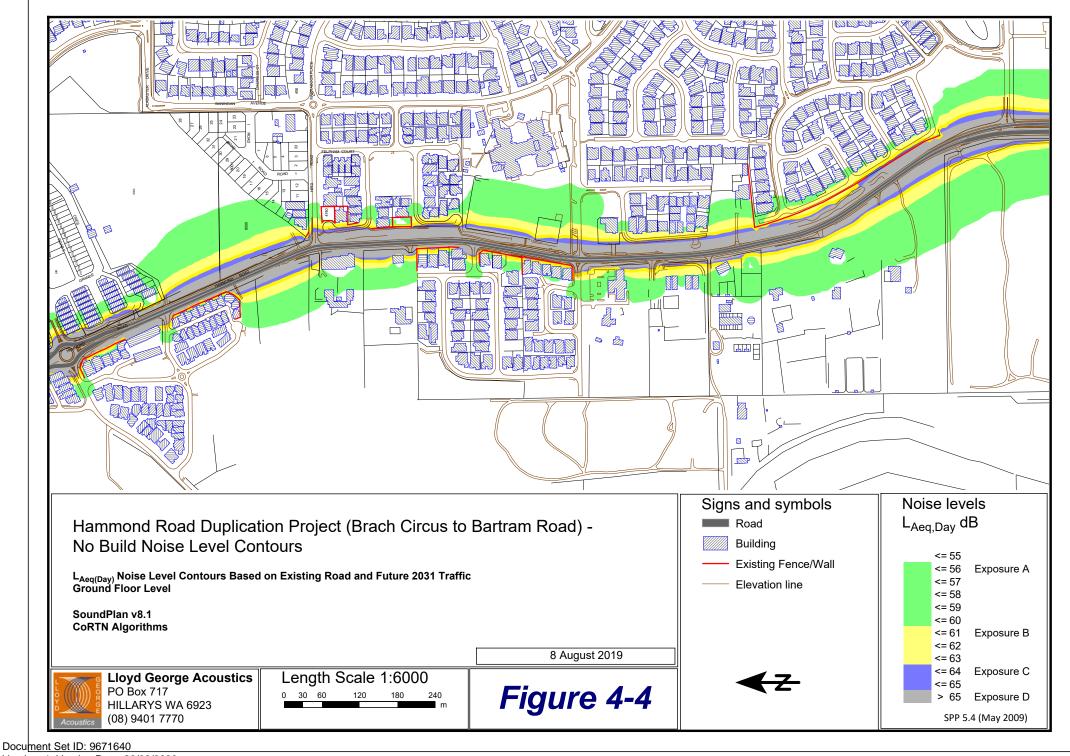
Address	Predicted L _{Aeq(Day)} , dB	Address	Predicted L _{Aeq(Day)} , dB
West Side Residences		East Side Residences	
01 Condil Way	61	8 Muirfield Avenue	61
03 Condil Way	61	10 Muirfield Avenue	60
05 Condil Way	59	12 Muirfield Avenue	61
07 Condil Way	59	14 Muirfield Avenue	62
09B Condil Way	60	16 Muirfield Avenue (Logger)	63
1/1 Modong Nook	60	18 Muirfield Avenue	63
2/1 Modong Nook	59	20 Muirfield Avenue	63

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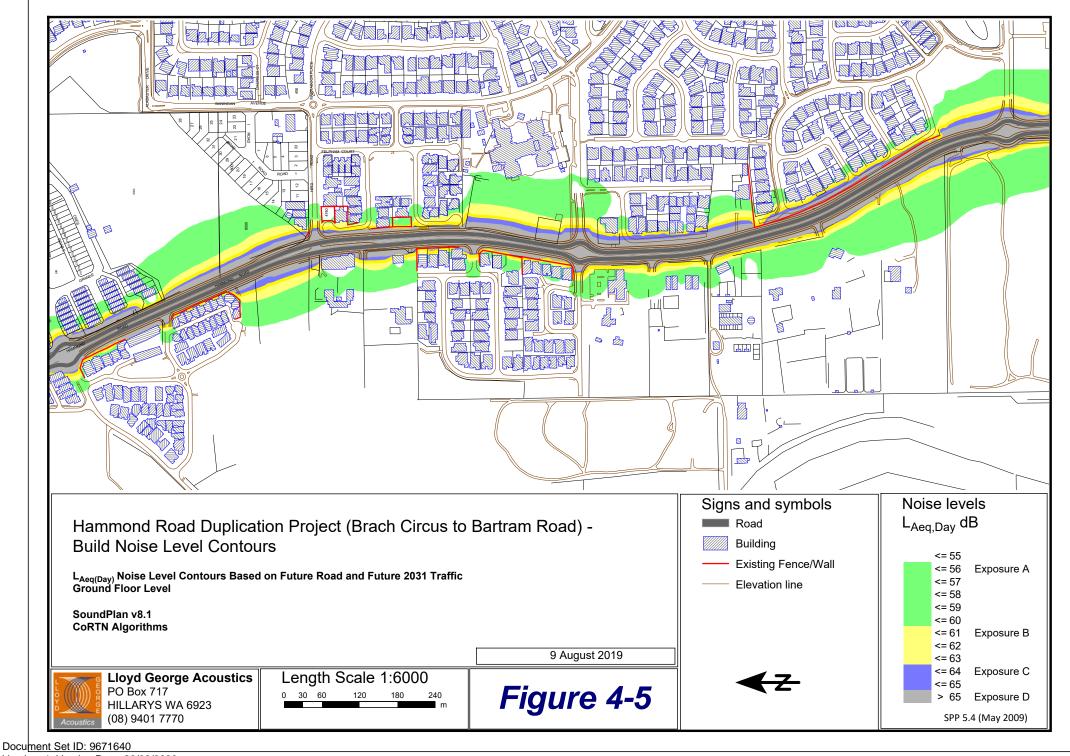
Address	Predicted L _{Aeq(Day)} , dB	Address	Predicted L _{Aeq(Day)} , dB
West Side Residences		East Side Residences	
3/1 Modong Nook	59	22 Muirfield Avenue	63
4/1 Modong Nook	59	24 Muirfield Avenue	63
5/1 Modong Nook	59	26 Muirfield Avenue	63
6/1 Modong Nook	59	28 Muirfield Avenue	62
7/1 Modong Nook	59	40 Carnegie Parade	62
8/1 Modong Nook	59	275 Hammond Road	58
9/1 Modong Nook	59	17 Joindre Way	64
9/1 Modong Nook	59	15 Joindre Way	64
210 Hammond Road	N/A	11B Joindre Way	64
222 Hammond Road	53	11A Joindre Way	64
30 Calytrix Crescent	60	09 Joindre Way	63
28 Calytrix Crescent	60	07 Joindre Way	63
26 Calytrix Crescent	60	05B Joindre Way	63
2 Aphelia Brace	62	05A Joindre Way	62
2 Aphelia Brace	63	08 Joindre Way Goodstart Early Learning	63
22 Calytrix Crescent	58	53 Baningan Avenue - Jandakot Primary	56
20 Calytrix Crescent	57	15 Makjanich Place	58
16 Calytrix Crescent	56	13 Makjanich Place	61
21 Wedgetail Crescent	57	11B Makjanich Place	61
25 Wedgetail Crescent	56	11A Makjanich Place	58
27 Wedgetail Crescent	57	12 Makjanich Place	56
272 Hammond Road	59	13 Gandossi Court	58
282 Hammond Road	55	13 Gandossi Court	63
300 Hammond Road	56	13 Gandossi Court	61
304 Hammond Road	54	12A Gandossi Court	58
		12A Gandossi Court	61
		14 Gandossi Court (Logger)	60
		01 Hird Road	60
		01 Hird Road	62
		01 Hird Road	60

Note: Numbers shown in Bold Red are above the *limit*.

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5 ASSESSMENT

For a road upgrade, SPP 5.4 states that practicable noise management and mitigation measures should be considered, having regard to —

- The existing transport noise levels;
- The likely change in noise emissions resulting from the proposal; and
- The nature and scale of the works and potential for noise amelioration.

From the above, there is no clear criteria for when noise mitigation is to occur. For the purposes of this assessment, the following has been used to identify potential areas where noise mitigation may be considered:

• Residences where the Build Scenario results in noise levels above the *limit* and an increase of more than 0.5 dB above the No Build Scenario.

Based on the above criteria guide, *Table 5-1* reviews each of the areas.

Table 5-1 Areas Considered For Noise Mitigation

Area	Comments	Image
Muirfield Avenue	Noise levels are calculated to be above the <i>limit</i> and increase by 1-3 dB compared to No Build and 4-6 dB compared to Existing. A retaining wall exists between Muirfield Avenue and the road project. A noise mitigation option would be to provide a new noise wall at a minimum height of 3.0 metres. Whilst the highlighted houses in the image are those that technically satisfy the nominated criteria, best practice would continue the wall further south to the end of Muirfield Avenue.	Constitution of the second of
Joindre Way	Noise levels are calculated to be above the <i>limit</i> and increase by 1-2 dB compared to No Build and 4-5 dB compared to Existing. Space exists between Joindre Way and the proposed alignment. A noise mitigation option would be to provide a wall in this location at a minimum height of 3.0 metres, relative to local road level. The childcare centre has driveway access and therefore the effectiveness of a noise wall may be limited.	AMERIC COT

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Area	Comments	Image
Gandossi Court	Noise levels are calculated to be above the <i>limit</i> and increase by 1 dB compared to the No Build and 4 dB compared to Existing. Whilst only 1 residence qualifies according to the nominated criteria, best practice would consider noise mitigation for all residences adjoining the road on Makjanich Place and Gandossi Court. Again, a noise wall may be practicable in this area, minimum 2.4 metres high, relative to the road design at the proposed location.	ANNOTATION OF THE PROPERTY OF

In each of the above, noise control put forward is in the form of noise walls. The modelling assumes the road surface is to remain unchanged (dense graded asphalt). This could be improved to stone mastic or open graded asphalt for reduced noise levels. The advantage of this approach is the noise reduction is achieved at all houses, however maintenance costs may be higher than that of noise walls.

It should be noted that there are other houses that have not been specifically assessed as part of this study, as they are relatively new and therefore noise mitigation would have been part of the development approvals process in the form of architectural upgrades. Such locations would be:

- Savant Grover;
- Jandari Mews
- Volta Way;
- 2 Coojong Link; and
- Windemere Circuit.

6 CONCLUSION

To satisfy the requirements of the *State Planning Policy 5.4 Road and Rail Transport Noise and Freight Considerations in Land Use Planning, Table 5-1* provides areas where noise mitigation is recommended where in each case, construction of a noise wall is considered practicable. The recommended heights are 2.4 to 3.0 metres, either relative to the proposed road or local road levels, depending on circumstances. Where a noise wall is to be provided, it is to be minimum 15kg/m² surface mass with no gaps.

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The three proposed walls are described as follows:

- Wall 1 Proposed to range in height from 3.0 metres to 4.5 metres at the southern end, relative to the provided design strings at the location shown in *Figure 6-1*. The residences are elevated compared to the proposed road and a retaining wall exists alongside the local road. City of Cockburn prefers not to modify the existing retaining wall. As such, the proposed wall is shown to follow the road design, although in reality may be built alongside the existing retaining wall to be determined in detailed design. The retaining wall increases towards the southern end, hence so too does the noise wall. Development to the south (Lot 858 Baningnan Avenue, Success) is expected to be providing their own wall and/or architectural packages). Total wall length is 330 metres with an approximate area of 1100m².
- Wall 2 Proposed to be 3.0 metres high, relative to the local road as shown in *Figure 6-1*, noting the residences are elevated above the local and proposed road. Total wall length is 139 metres with a total area of approximately 420m².
- Wall 3 Proposed to be 2.4 metres high, relative to the provided design strings at the location shown in *Figure 6-1*, noting the road is elevated compared to the residences. Total wall length is 212 metres with a total area of approximately 510m².

A limestone noise wall has an indicative cost of \$120/m², being around \$240,000 for all 3 walls.

Table 6-1 provides the predicted noise levels at the three wall locations and the noise reduction provided.

Table 6-1 Predicted L_{Aeq(Day)} Noise Levels With Proposed Wall and Noise Reduction

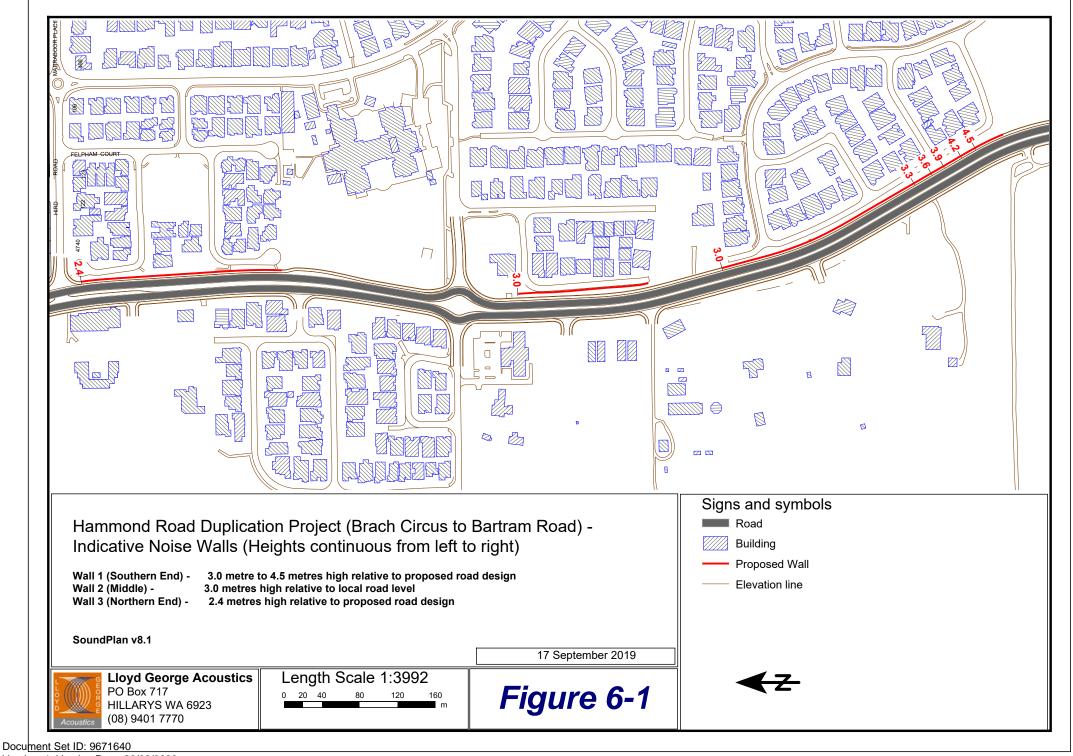
Address	Predicted L _{Aeq(Day)} , dB	Noise reduction		
Wall 1				
8 Muirfield Avenue	58	2.8		
10 Muirfield Avenue	56	4.4		
12 Muirfield Avenue	54	6.6		
14 Muirfield Avenue	54	7.1		
16 Muirfield Avenue (Logger)	55	7.8		
18 Muirfield Avenue	55	8.2		
20 Muirfield Avenue	55	8.2		
22 Muirfield Avenue	54	8.7		
24 Muirfield Avenue	55	8.7		
26 Muirfield Avenue	55	8.4		
28 Muirfield Avenue	54	7.9		
40 Carnegie Parade	56	5.6		

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Address	Predicted L _{Aeq(Day)} , dB	Noise reduction		
	Wall 2			
17 Joindre Way	62	2.4		
15 Joindre Way	58	6.5		
11B Joindre Way	57	7.5		
11A Joindre Way	56	7.8		
09 Joindre Way	55	8.0		
07 Joindre Way	56	7.8		
05B Joindre Way	54	8.4		
05A Joindre Way	58	4.6		
	Wall 3			
15 Makjanich Place	55	3.8		
13 Makjanich Place	55	6.2		
11B Makjanich Place	55	6.6		
11A Makjanich Place	52	6.0		
12 Makjanich Place	51	4.8		
13 Gandossi Court	52	5.7		
13 Gandossi Court	54	8.3		
13 Gandossi Court	54	7.7		
12A Gandossi Court	52	6.4		
12A Gandossi Court	56	5.1		
14 Gandossi Court (Logger)	55	4.7		

Noise Reduction is the difference between Future Build (Table 4-6) and with Future Build with Noise Walls

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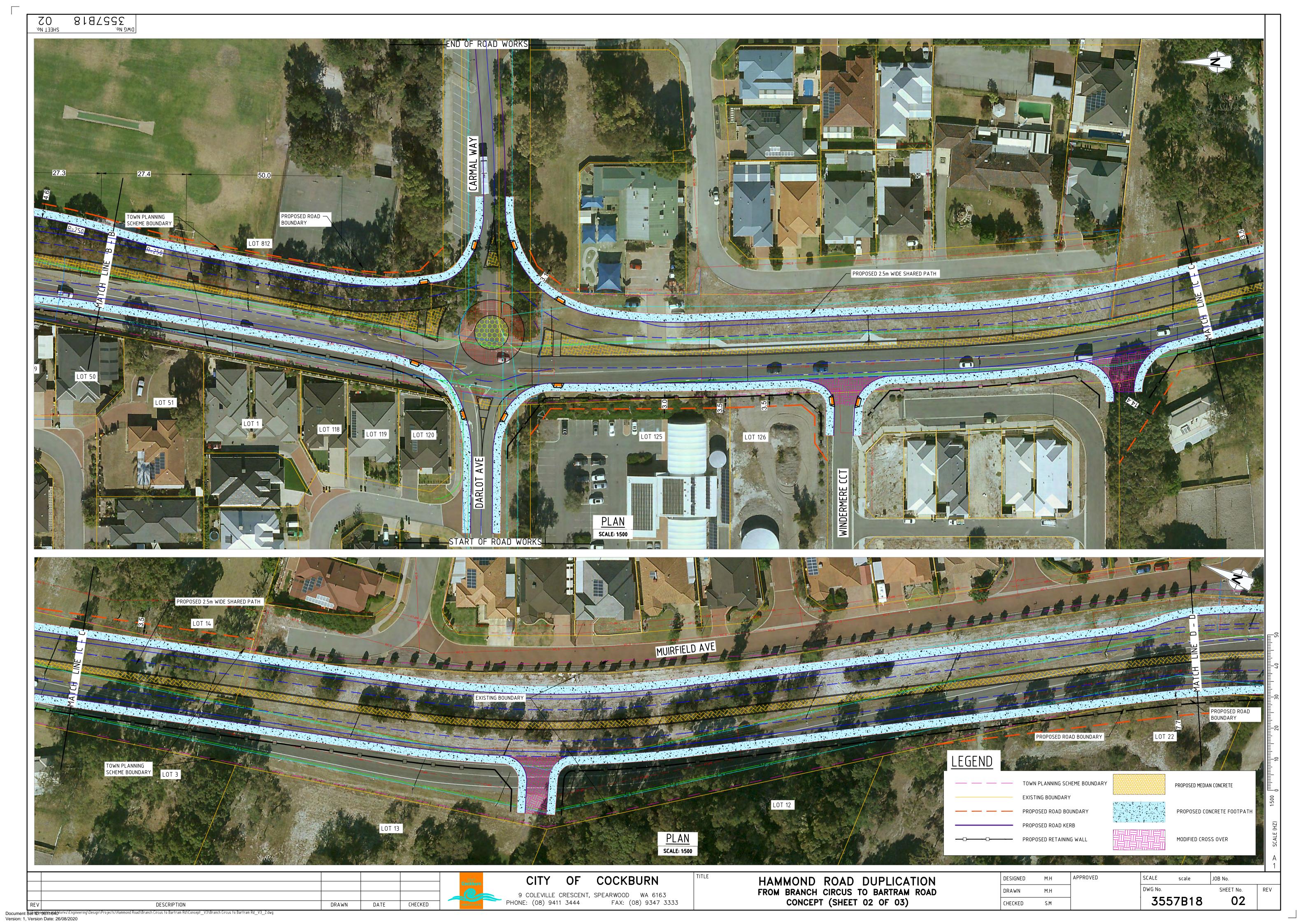
Version: 1, Version Date: 26/08/2020

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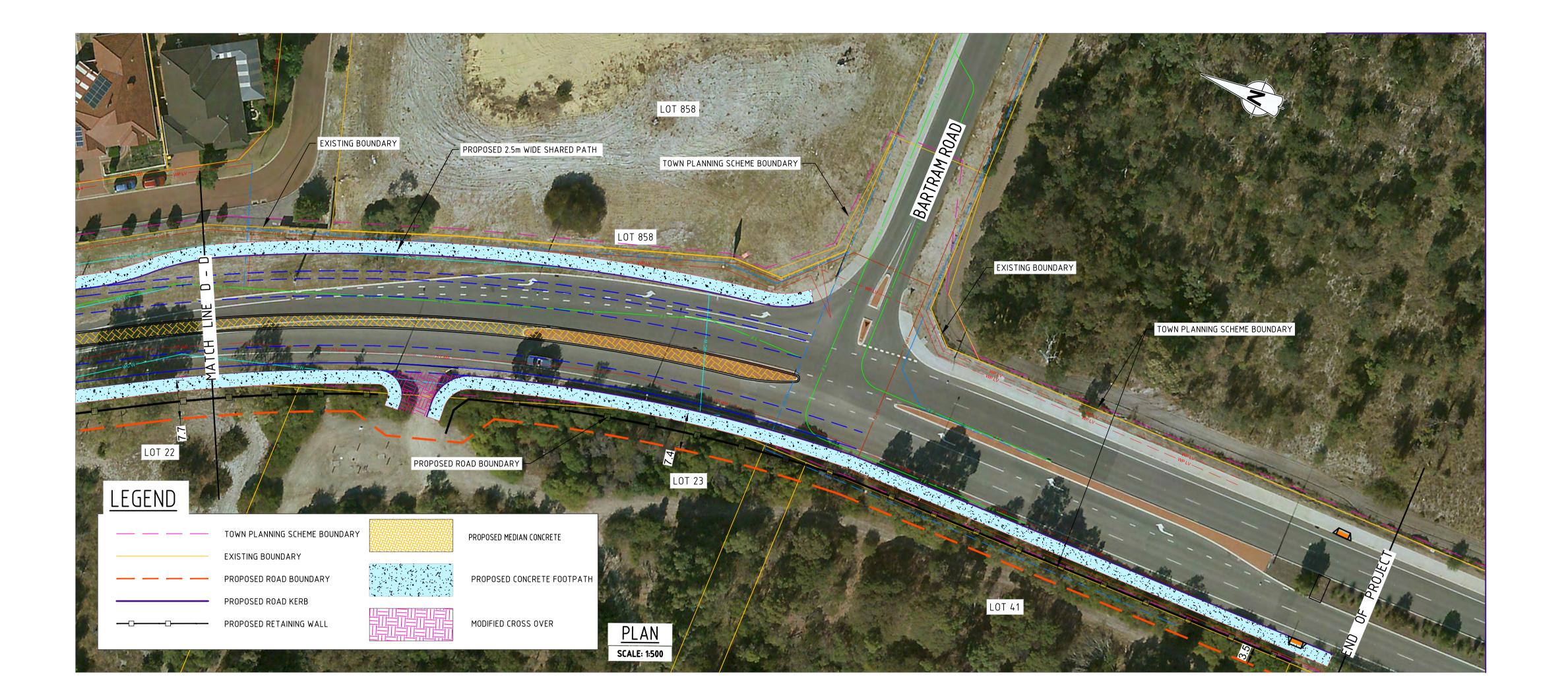
Appendix A

Proposed Road Design





2257B18 03



A T SCALE (HZ) 1:500

REV DESCRIPTION DRAWN DATE CHECKED

City of Cockburn

Wetlands to waves

CITY OF COCKBURN

9 COLEVILLE CRESCENT, SPEARWOOD WA 6163
PHONE: (08) 9411 3444 FAX: (08) 9347 3333

HAMMOND ROAD DUPLICATION FROM BRANCH CIRCUS TO BARTRAM ROAD CONCEPT (SHEET 03 OF 03)

DESIGNED M.H APPROVED SCALE Scale JOB No.

DRAWN M.H

CHECKED S.M

SCALE Scale JOB No.

SHEET No.

3557B18

O3

Document Set note: 26/08/2020

Document Set note: 26/08/2020

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Appendix B

Terminology

The following is an explanation of the terminology used throughout this report.

Decibel (dB)

The decibel is the unit that describes the sound pressure and sound power levels of a noise source. It is a logarithmic scale referenced to the threshold of hearing.

A-Weighting

An A-weighted noise level has been filtered in such a way as to represent the way in which the human ear perceives sound. This weighting reflects the fact that the human ear is not as sensitive to lower frequencies as it is to higher frequencies. An A-weighted sound level is described as L_A dB.

L₁

An L₁ level is the noise level which is exceeded for 1 per cent of the measurement period and is considered to represent the average of the maximum noise levels measured.

L₁₀

An L_{10} level is the noise level which is exceeded for 10 per cent of the measurement period and is considered to represent the "intrusive" noise level.

L₉₀

An L_{90} level is the noise level which is exceeded for 90 per cent of the measurement period and is considered to represent the "background" noise level.

Lea

The L_{eq} level represents the average noise energy during a measurement period.

L_{A10,18hour}

The $L_{A10,18 \text{ hour}}$ level is the arithmetic average of the hourly L_{A10} levels between 6.00 am and midnight. The *CoRTN* algorithms were developed to calculate this parameter.

L_{Aeq,24hour}

The $L_{Aeq,24\,hour}$ level is the logarithmic average of the hourly L_{Aeq} levels for a full day (from midnight to midnight).

L_{Aeq,8hour} / L_{Aeq (Night)}

The $L_{Aeq (Night)}$ level is the logarithmic average of the hourly L_{Aeq} levels from 10.00 pm to 6.00 am on the same day.

L_{Aeq,16hour} / L_{Aeq (Day)}

The $L_{Aeq (Day)}$ level is the logarithmic average of the hourly L_{Aeq} levels from 6.00 am to 10.00 pm on the same day. This value is typically 1-3 dB less than the $L_{A10.18hour}$.

Satisfactory Design Sound Level

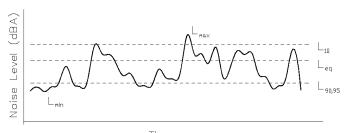
The level of noise that has been found to be acceptable by most people for the environment in question and also to be not intrusive.

Maximum Design Sound Level

The level of noise above which most people occupying the space start to become dissatisfied with the level of noise.

Reference: 19055001-01.docx Page B1

Chart of Noise Level Descriptors



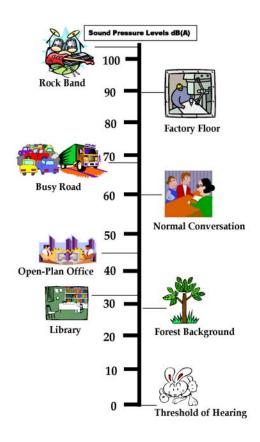
Time

Austroads Vehicle Class

AUSTROADS Vehicle Classification System

Axies Axie G Axies	roups	Vehicle Type Typical Description	1		AUSTROADS Classification
		Topical Description			
Axles	Groups				
			Class	Parameters	Typical Configuration
	LIGHT VEHICLES				
		Short			
	1 or 2	Sedan, Wagon, 4WD, Utility, Light Van, Bioyole, Motorcycle, etc.	1	d(1) ≤ 3.2m and axies = 2	
		Short - Towing		groups = 3	(C 2 C C C C C C C C C C C C C C C C C
3, 4 or 5	3	Trailer, Caravan, Boat, etc	2	$d(1) \ge 2.1m$, $d(1) \le 3.2m$, $d(2) \ge 2.1m$ and axies = 3, 4 or 5	
				HEAVY VEHIC	CLES
2	2	Two Axle Truck or Bus	3	d(1) > 3.2m and axies = 2	
3	2	Three Axle Truck or Bus	4	axies = 3 and groups = 2	
> 3	2	Four Axle Truck	5	axies > 3 and groups = 2	
3	3	Three Axle Articulated Three axle articulated vehicle, or Rigid vehicle and trailer	6	d(1) > 3.2m, aides = 3 and groups = 3	
4	Þ 2	Four Axle Articulated Four axle articulated vehicle, or Rigid vehicle and trailer	7	d(2) < 2.1m or d(1) < 2.1m or d(1) > 3.2m axles = 4 and groups > 2	
5	> 2	Five Axle Articulated Five axle articulated vehicle, or Rigid vehicle and trailer	8	d(2) < 2.1m or d(1) < 2.1m or d(1) > 3.2m astes = 5 and groups > 2	
≥6	> 2	Six Axle Articulated Six axle articulated vehicle, or Rigid vehicle and trailer	9	axies = 6 and groups > 2 or axies > 6 and groups = 3	
> 6	4	B Double B Double, or Heavy truck and trailer	10	groups = 4 and axies > 6	
>6	5 or 6	Double Road Train Double road train, or Medium articulated vehicle and one dog trailer (M.A.D.)	11	groups = 5 or 6 and axles > 6	
> 6	> 6	Triple Road Train Triple road train, or Heavy truck and three trailers	12	groups > 6 and axles > 6	
	2 3 >3 3 4 5 >6 >6 >6 >7 >7 >7 >7 >7 >7 >7 >7 >7 >7 >7 >7 >7	2 2 2 3 2 2 3 3 3 4 5 2 5 5 5 2 2 5 6 5 6 5 6 6 5 6 6 5 6 6 5 6 6 5 6 6 5 6 6 5 6 6 5 6 6 5 6 6 5 6 6 5 6 6 5 6 6 5 6 6 5 6 6 6 5 6 6 6 5 6 6 6 5 6 6 6 5 6 6 6 5 6 6 6 5 6 6 6 5 6	2 2 Two Aris Truck or Bus 2 2 Two Aris Truck or Bus 3 2 These Aris Truck or Bus 3 2 These Aris Truck or Bus 3 3 These Aris Truck or Bus 4 5 Prior Aris Truck 5 3 These Aris Truck or Bus 5 5 Prior Aris Afficialisted 6 7 Prior aris and Confession of Confession 6 7 Prior aris and Confession of Confession 7 Prior aris and Confession of Confession 7 Prior aris and Confession of Confession 8 Prior aris and Confession 8 Prior aris and Confession 9 Prior	1,4 or 2 Transe Carrenn, Bord, etc. 2	4 of 5 3 Trader, Calman, Book eta 2 (d1) > 2 m, (d1) > 2

Typical Noise Levels



Reference: 19055001-01.docx Page B2